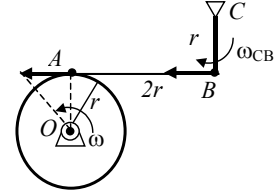


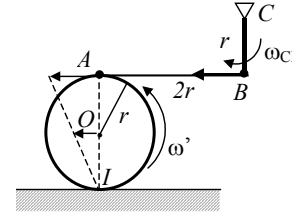
$$\mathbf{1.a} \quad \left. \begin{aligned} \vec{v}_A &= \vec{v}_O + \vec{\omega} \times \vec{OA} = \vec{\omega}_{OA} \times \vec{OA} = \omega_{OA} r \vec{1}_x \\ \vec{v}_B &= \vec{v}_C + \vec{\omega}_{CB} \times \vec{CB} = \omega_{CB} r \vec{1}_x \end{aligned} \right\} \Rightarrow \omega = \omega_{CB}$$

Les vitesses v_A et v_B sont parallèles. Comme la barre AB est indéformable, elle subit une translation curviligne instantanée donc les vitesses de A et B doivent être égales.



$$\mathbf{1.b} \quad \left. \begin{aligned} \vec{v}_A &= \vec{v}_I + \vec{\omega}' \times \vec{IA} = \vec{\omega}' \times \vec{IA} = \omega' 2r \vec{1}_x \\ \vec{v}_B &= \vec{v}_C + \vec{\omega}_{CB} \times \vec{CB} = \omega_{CB} r \vec{1}_x \end{aligned} \right\} \Rightarrow 2\omega' = \omega_{CB}$$

(avec I le point de contact du disque avec le sol)



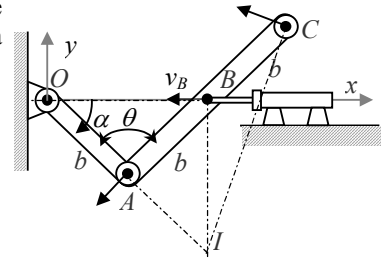
2.1 Le CIR de la barre OA est O et celui de la barre AC est représenté sur le dessin : I (intersection de la droite perpendiculaire à v_A et de la perpendiculaire à v_B).

$$A \in \text{solide } OA : \alpha = \frac{\pi}{2} - \frac{\theta}{2} \Rightarrow \dot{\alpha} = -\frac{\dot{\theta}}{2}$$

$$\vec{v}_A = \vec{v}_O + \vec{\omega}_{OA} \times \vec{OA} = -\dot{\alpha} b \left(\cos \frac{\theta}{2} \vec{1}_x + \sin \frac{\theta}{2} \vec{1}_y \right) = \frac{\dot{\theta}}{2} b \left(\cos \frac{\theta}{2} \vec{1}_x + \sin \frac{\theta}{2} \vec{1}_y \right)$$

$$A \in \text{solide } AB : \vec{v}_A = \vec{v}_B + \vec{\omega}_{AC} \times \vec{BA} = -v_b \vec{1}_x + \omega b \left(\cos \frac{\theta}{2} \vec{1}_x - \sin \frac{\theta}{2} \vec{1}_y \right)$$

$$\left. \begin{aligned} b \cos \frac{\theta}{2} \frac{\dot{\theta}}{2} &= -v_b + b \cos \frac{\theta}{2} \omega \\ b \sin \frac{\theta}{2} \frac{\dot{\theta}}{2} &= -b \sin \frac{\theta}{2} \omega \end{aligned} \right\} \Rightarrow \omega = -\frac{\dot{\theta}}{2} \text{ d'où } v_b = -b \dot{\theta} \cos \frac{\theta}{2} \Rightarrow \vec{v}_C = \vec{v}_A + \vec{\omega}_{AC} \times \vec{AC} = v_b \left(-\frac{3}{2} \vec{1}_x + \frac{1}{2} \tan \frac{\theta}{2} \vec{1}_y \right)$$



$$\mathbf{2.2} \quad \vec{v}_B = -v_b \vec{1}_x = \frac{d}{dt} \left(2b \sin \frac{\theta}{2} \right) \vec{1}_x = b \cos \frac{\theta}{2} \dot{\theta} \vec{1}_x \Rightarrow v_b = -b \cos \frac{\theta}{2} \dot{\theta}$$

$$\left\{ \begin{aligned} x_C &= b \sin \frac{\theta}{2} + 2b \sin \frac{\theta}{2} = 3b \sin \frac{\theta}{2} \\ y_C &= b \cos \frac{\theta}{2} \end{aligned} \right\} \Rightarrow \left\{ \begin{aligned} \dot{x}_C &= \frac{3b}{2} \cos \frac{\theta}{2} \dot{\theta} = -\frac{3}{2} v_b \\ \dot{y}_C &= -\frac{b}{2} \sin \frac{\theta}{2} \dot{\theta} = \frac{1}{2} v_b \tan \frac{\theta}{2} \end{aligned} \right\} \Rightarrow \vec{v}_C = v_b \left(-\frac{3}{2} \vec{1}_x + \frac{1}{2} \tan \frac{\theta}{2} \vec{1}_y \right)$$

$$\mathbf{3} \quad \vec{v}_B = \frac{r}{2} \pi \vec{1}_x \quad (\vec{\omega}_{BC} = -\pi \text{ rad/s } \vec{1}_z; \vec{\omega}_{OA} = -\omega_{OA} \vec{1}_z \text{ et } \vec{\omega}_{BA} = -\omega_{BA} \vec{1}_z)$$

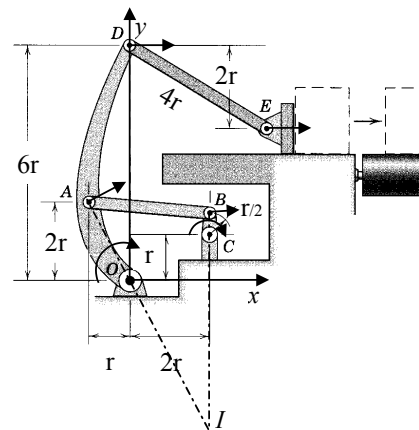
$$\left\{ \begin{aligned} \vec{v}_A &= \vec{v}_O + \vec{\omega}_{OA} \times \vec{OA} = 2r\omega_{OA} \vec{1}_x + r\omega_{OA} \vec{1}_y \\ \vec{v}_A &= \vec{v}_B + \vec{\omega}_{BA} \times \vec{BA} = \left(\frac{r}{2} \pi + \frac{r}{2} \omega_{BA} \right) \vec{1}_x + 3r\omega_{BA} \vec{1}_y \end{aligned} \right.$$

$$\Rightarrow \omega_{OA} = 3\omega_{BA} ; \vec{\omega}_{BA} = -\frac{\pi}{11} \text{ rad/s } \vec{1}_z \text{ et } \vec{\omega}_{OA} = -\frac{3\pi}{11} \text{ rad/s } \vec{1}_z$$

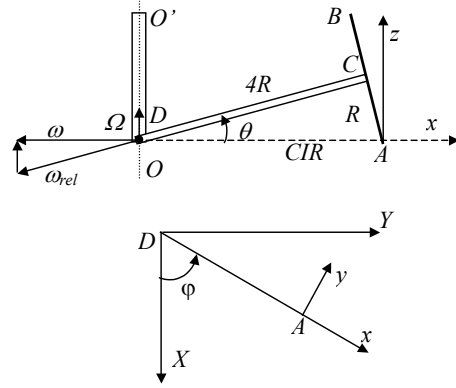
$$\vec{v}_D = \vec{v}_O + \vec{\omega}_{OA} \times \vec{OD} = \frac{3\pi}{11} \cdot 6r \vec{1}_x$$

$$\vec{v}_E = \vec{v}_D + \vec{\omega}_{DE} \times \vec{DE} = \frac{18\pi r}{11} \vec{1}_x + 2r\omega_{DE} \vec{1}_x + 2\sqrt{3}r\omega_{DE} \vec{1}_y = v_E \vec{1}_x$$

$$\Rightarrow \omega_{DE} = 0 \text{ (barre en translation instantanée) et } \vec{v}_E = \frac{18\pi r}{11} \vec{1}_x$$



4.1 Nous repérons deux points appartenant au solide qui ont une vitesse nulle : le disque ne glisse pas donc la vitesse du point A est nulle. Il en est de même pour le point D qui est appartenant à l'axe fixe OO' . Donc l'axe instantané de rotation passe bien par ses deux points.



$$\vec{\omega} = \vec{\Omega} + \vec{\omega}_{rel} = -\omega_{rel} \cos \theta \vec{I}_x + (\Omega - \omega_{rel} \sin \theta) \vec{I}_z$$

Condition de roulement sans glissement :

$$\vec{v}_A = 0 = \vec{v}_C + \vec{\omega} \times \vec{CA} \quad \text{avec} \quad \vec{CA} = R \sin \theta \vec{I}_x - R \cos \theta \vec{I}_z$$

$$\text{et} \quad \vec{v}_C = \vec{\Omega} \times \vec{OC} = \Omega 4R \cos \theta \vec{I}_y$$

$$\vec{v}_A = 0 = \Omega 4R \cos \theta \vec{I}_y + (\Omega R \sin \theta - \omega_{rel} R) \vec{I}_y$$

$$\Rightarrow \Omega 4R \cos \theta + R \Omega \sin \theta - R \omega_{rel} = 0$$

$$\omega_{rel} = \Omega \sqrt{17} \quad \text{par le dessin on peut aussi directement établir que} \quad \frac{\Omega}{\omega} = \tan \theta \quad \text{et} \quad \omega_{rel} = \frac{\omega}{\cos \theta}$$

$$\Rightarrow \vec{\omega} = -\Omega \sqrt{17} \cos \theta \vec{I}_x + \Omega (1 - \sqrt{17} \sin \theta) \vec{I}_z = -4\Omega \vec{I}_x \quad \text{et} \quad \vec{\varepsilon} = \vec{\Omega} \times \vec{\omega} = \Omega \vec{I}_z \times \vec{\omega} = -4\Omega^2 \vec{I}_y$$

4.2

$$\vec{v}_B = \vec{\omega} \times \vec{AB} = -4\Omega \vec{I}_x \times 2R (-\sin \theta \vec{I}_x + \cos \theta \vec{I}_z) = \frac{32\sqrt{17}}{17} \Omega R \vec{I}_y \quad \text{ou} \quad \vec{v}_B = \left. \frac{d\vec{DB}}{dt} \right|_{abs} = \left. \frac{d\vec{DB}}{dt} \right|_{rel} + \vec{\Omega} \times \vec{DB}$$

$$\vec{a}_A = \vec{a}_C + \vec{\varepsilon} \times \vec{CA} + \vec{\omega} \times (\vec{\omega} \times \vec{CA}) = \frac{68}{\sqrt{17}} R \Omega^2 \vec{I}_z \quad \text{où} \quad \vec{a}_C = \underbrace{\vec{a}_D}_{=0} + \underbrace{\vec{\varepsilon} \times \vec{DC}}_{=0} + \vec{\Omega} \times (\vec{\Omega} \times \vec{DC}) = -\Omega^2 4R \cos \theta \vec{I}_x$$

$$\vec{a}_B = \vec{a}_A + \vec{\varepsilon} \times \vec{AB} + \vec{\omega} \times (\vec{\omega} \times \vec{AB}) = \frac{68}{\sqrt{17}} R \Omega^2 \vec{I}_z - 4\Omega^2 \vec{I}_y \times 2R (-\sin \theta \vec{I}_x + \cos \theta \vec{I}_z) - 4\Omega \vec{I}_x \times \frac{32\sqrt{17}}{17} \Omega R \vec{I}_y$$

$$\vec{a}_B = \frac{68}{\sqrt{17}} R \Omega^2 \vec{I}_z - \frac{8}{\sqrt{17}} \Omega^2 R \vec{I}_z - \frac{32}{\sqrt{17}} \Omega^2 R \vec{I}_x - \frac{128}{\sqrt{17}} \Omega^2 R \vec{I}_z = -\frac{32}{\sqrt{17}} \Omega^2 R \vec{I}_x - \frac{68}{\sqrt{17}} \Omega^2 R \vec{I}_z$$

$$\text{ou} \quad \vec{a}_B = \left. \frac{d\vec{v}_B}{dt} \right|_{abs} = \left. \frac{d\vec{v}_B}{dt} \right|_{rel} + \vec{\Omega} \times \vec{v}_B = -\frac{68}{\sqrt{17}} R \Omega^2 \vec{I}_z - \frac{32\sqrt{17}}{17} R \Omega^2 \vec{I}_x$$

5. 1. OS Horizontal : (AS est parallèle à l'axe y)

$$\sin 60.6 - \sin 60.4 = \frac{\sqrt{3}}{2} \cdot 2 \Rightarrow AC = \frac{\sqrt{3}}{\sin 30} = 2\sqrt{3} \text{ m}$$

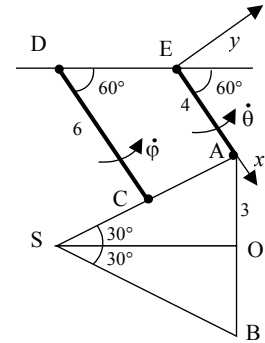
2. Vitesse angulaire de la barre DC

$$\dot{\theta} = 3 \text{ rad/s} \vec{I}_z \quad \text{et} \quad \dot{\phi} ?$$

$$\vec{v}_C // \vec{v}_A \Rightarrow \text{le triangle est en translation instantanée : } \vec{\omega}_{AC} = 0 \text{ et } \vec{v}_C = \vec{v}_A$$

$$\vec{v}_A = \underbrace{\vec{v}_E}_0 + \dot{\theta} \vec{I}_z \times \vec{EA} = 4\dot{\theta} \vec{I}_y \quad \text{et} \quad \vec{v}_C = \underbrace{\vec{v}_D}_0 + \vec{\omega}_{DC} \times \vec{DC} = 6\dot{\phi} \text{ m/s} \vec{I}_y \Rightarrow \dot{\phi} = 2 \text{ rad/s} \vec{I}_z$$

3. Vitesse et accélération du point S



$$\vec{v}_S = \vec{v}_C = \vec{v}_A = 12 \text{ m/s} \vec{I}_y \quad \text{et} \quad \vec{a}_S = \vec{a}_A + \vec{\varepsilon}_{SA} \times \vec{AS} + \vec{\omega}_{SA} \times (\vec{\omega}_{SA} \times \vec{AS}) = \vec{a}_A + \vec{\varepsilon}_{SA} \times \vec{AS}$$

$$\vec{a}_A = \vec{a}_E + \vec{\varepsilon}_{AE} \times \vec{EA} + \vec{\omega}_{EA} \times (\vec{\omega}_{EA} \times \vec{EA}) = \vec{\omega}_{EA} \times (\vec{\omega}_{EA} \times \vec{EA}) = -\omega_{EA}^2 \vec{EA} = -\|\vec{EA}\| \dot{\theta}^2 \vec{I}_x = -4\dot{\theta}^2 \vec{I}_x$$

$$\begin{cases} \vec{a}_{C(C \in AC)} = \vec{a}_A + \vec{\varepsilon}_{AC} \times \vec{AC} + \underbrace{\vec{\omega}_{AC} \times (\vec{\omega}_{AC} \times \vec{AC})}_{=0} = -\|\vec{EA}\| \dot{\theta}^2 \vec{I}_x + \|\vec{AC}\| \varepsilon_{AC} \vec{I}_x \\ \vec{a}_{C(C \in AD)} = \underbrace{\vec{a}_D}_0 + \vec{\varepsilon}_{DC} \times \vec{DC} + \vec{\omega}_{DC} \times (\vec{\omega}_{DC} \times \vec{DC}) = \|\vec{DC}\| \varepsilon_{DC} \vec{I}_y - \|\vec{DC}\| \dot{\phi}^2 \vec{I}_x \end{cases}$$

$$\Rightarrow \varepsilon_{DC} = 0 \quad \text{et} \quad -\|\vec{EA}\| \dot{\theta}^2 + \varepsilon_{AC} \|\vec{AC}\| = -\|\vec{DC}\| \dot{\phi}^2 \Rightarrow \varepsilon_{AC} = \frac{\|\vec{EA}\| \dot{\theta}^2 - \|\vec{DC}\| \dot{\phi}^2}{\|\vec{AC}\|} = \frac{4 \cdot 3^2 - 6 \cdot 2^2}{2\sqrt{3}} = 2\sqrt{3} \text{ m/s}^2 \vec{I}_z$$

$$\Rightarrow \vec{a}_S = \vec{a}_A + \vec{\varepsilon}_{SA} \times \vec{AS} = \left(-4\dot{\theta}^2 + 2\sqrt{3} \cdot \frac{3}{\sin 30} \right) \vec{I}_x = 12(-3 + \sqrt{3}) \vec{I}_x$$